

1 Nanofiltration Membranes with Crumpled Polyamide Films: A Critical
2 Review on Mechanisms, Performances, and Environmental Applications

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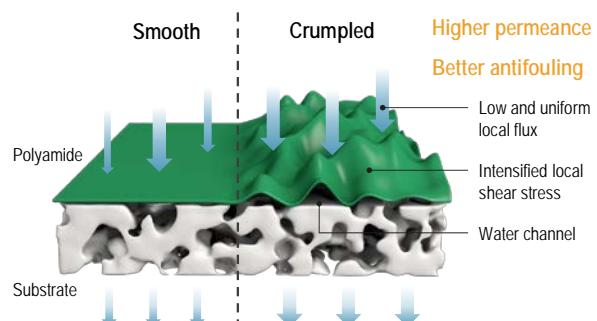
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34 **NOTES**

35 The authors declare no competing financial interest.



38 ■ ABSTRACT

39 Nanofiltration (NF) membranes have been widely applied in many important environmental
40 applications including water softening, surface/ground water purification, wastewater treatment,
41 and water reuse. In recent years, a new class of piperazine (PIP)-based NF membranes featuring
42 a crumpled polyamide layer has received considerable attention due to their great potential for
43 achieving dramatic improvements in membrane separation performance. Since the report of
44 novel crumpled Turing structures that exhibited an order magnitude enhancement in water
45 permeance (*Science* 360(6388), 518-521, 2018), the number of published research papers on this
46 emerging topic has grown exponentially to approximately 200. In this critical review, we provide
47 a systematic framework to classify the crumpled NF morphologies. The fundamental
48 mechanisms and fabrication methods involved in the formation of these crumpled morphologies
49 are summarized. We then discuss the transport of water and solutes in crumpled NF membranes
50 and how these transport phenomena could simultaneously improve membrane water permeance,
51 selectivity, and anti-fouling performance. The environmental applications of these emerging NF
52 membranes are highlighted, and future research opportunities/needs are identified. The
53 fundamental insights in this review provide critical guidance on the further development of high-
54 performance NF membranes tailored for a wide range of environmental applications.

55

56 **Keywords:** Nanofiltration, Polyamide, Crumpled morphology, Water transport pathway,
57 Selectivity, Membrane fouling

58 **Synopsis:** Nanofiltration membranes with well-controlled morphologies have the potential to
59 simultaneously improve water permeance, selectivity, and anti-fouling ability.

60

61 ■ INTRODUCTION

62 Nanofiltration (NF) is a pressure-driven membrane process that has separation abilities between
63 ultrafiltration (UF) and reverse osmosis (RO). A typical NF membrane has a molecular weight
64 cut-off between 150 and 2000 Da and is efficient in rejecting multivalent ions and organic
65 compounds.^{1, 2} Therefore, NF technology has been widely adopted in drinking water
66 purification,³ wastewater reclamation,^{4, 5} water softening,^{3, 6} food processing,⁷ pharmaceutical
67 industry,⁸ etc. Unlike seawater, the feed water in these applications generally has relatively low
68 osmotic pressures; thus, increasing the permeance of NF membranes could significantly improve
69 water production and reduce energy consumption.^{9, 10} However, membrane separation
70 performance is constrained by the permeance -selectivity tradeoff: highly permeable membranes
71 typically have low rejections to target substances and vice versa.¹¹⁻¹⁴ Consequently, it is a major
72 challenge to improve the permeance of NF membrane without compromising selectivity.

73

74 Currently, the gold standard for commercially available NF membranes is thin-film composite
75 (TFC) polyamide membranes, which are composed of a polyamide rejection layer, a UF
76 substrate, and a non-woven fabric support.¹⁵⁻¹⁷ The polyamide rejection layers of NF membranes
77 are often prepared by interfacial polymerization, with piperazine (PIP) and trimesoyl chloride
78 (TMC) as the most used monomers.^{13, 15, 16} It should be noted that the NF membrane in this
79 review, thus, specifically refers to the TFC polyamide membrane prepared using interfacial
80 polymerization reaction with PIP and TMC. With numerous in-depth studies on the polyamide
81 selective layer formed by the interfacial polymerization reaction, the morphology of the
82 polyamide layer is found to have a significant influence on the permeance of TFC membranes.
83 For example, in RO membranes formed by *m*-phenylenediamine (MPD) and TMC (Fig. 1a), the

84 “ridge-and-valley” morphology of the formed polyamide layer greatly improves the permeance
85 of RO membrane by increasing the effective filtration area¹⁸⁻²⁰ and creating voids in the
86 polyamide layer,^{18, 20-25} whose self-guttering effect further improves membrane permeance.^{20, 26-}
87 ²⁸ Unlike RO membranes, commercially available NF membranes formed by PIP and TMC are
88 relatively smooth (Fig. 1a). Inspired by the highly efficient water transport in TFC RO
89 membranes,^{18, 19} one may wonder if NF membranes with crumpled polyamide layers may
90 effectively enhance water permeance over their smooth counterparts to overcome the permeance
91 -selectivity tradeoff.

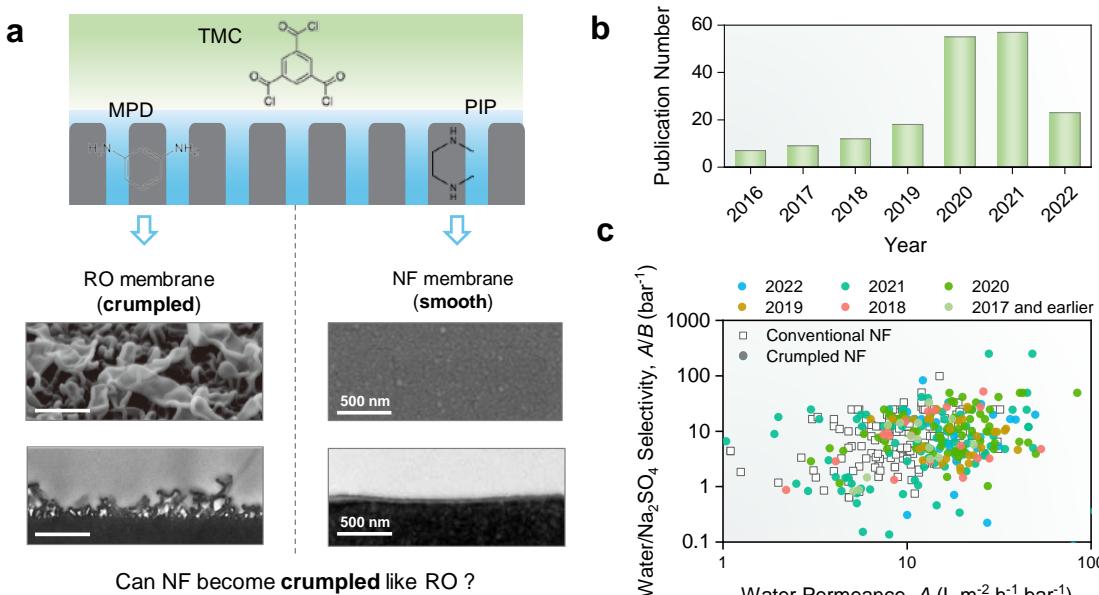
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93 In recent years, PIP-based NF membranes with crumpled polyamide layers have received
94 considerable attention (Fig. 1b). Particularly followed by the seminal work of Turing structure in
95 *Science* in 2018,²⁹ the number of publications on crumpled NF membranes is rapidly growing.
96 Researchers have developed various methods to fabricate NF membranes with different surface
97 morphologies (Table S1), along with major enhancement of water permeance from ~10 to >20
98 LMH/bar, pushing the separation performance (e.g., water-Na₂SO₄ selectivity (A/B) vs. water
99 permeance (A)) towards the top right corner in the upper bound diagram (Fig. 1c). Despite such
100 promising progress in crumple NF membranes, a dedicated review on the formation of and
101 transport of this emerging type of membranes is not yet available. More importantly, the
102 underlying mechanisms (e.g., how the crumpled morphologies affect the transport of water and
103 solutes) have yet to be systematically examined. In addition, the related fouling behavior of
104 crumpled NF membranes has not been fully understood.

105

106 Therefore, to better facilitate the in-depth understanding of crumpled NF membranes, this critical
 107 review summarizes their recent progress, with particular emphasis on 1) a systematic framework
 108 to classify the crumpled NF morphologies, 2) fundamental mechanisms and fabrication methods
 109 involved in the formation of these crumpled morphologies, 3) transport mechanisms of water and
 110 solutes in crumpled NF membranes, and 4) fouling propensities of crumpled NF membranes.
 111 The critical insights and important design criteria gained in this review facilitate the development
 112 of more efficient environmental applications with high energy efficiency and/or better anti-
 113 fouling properties. This review also identifies the critical research gaps and research
 114 opportunities pertaining to the further development of crumpled NF membrane.

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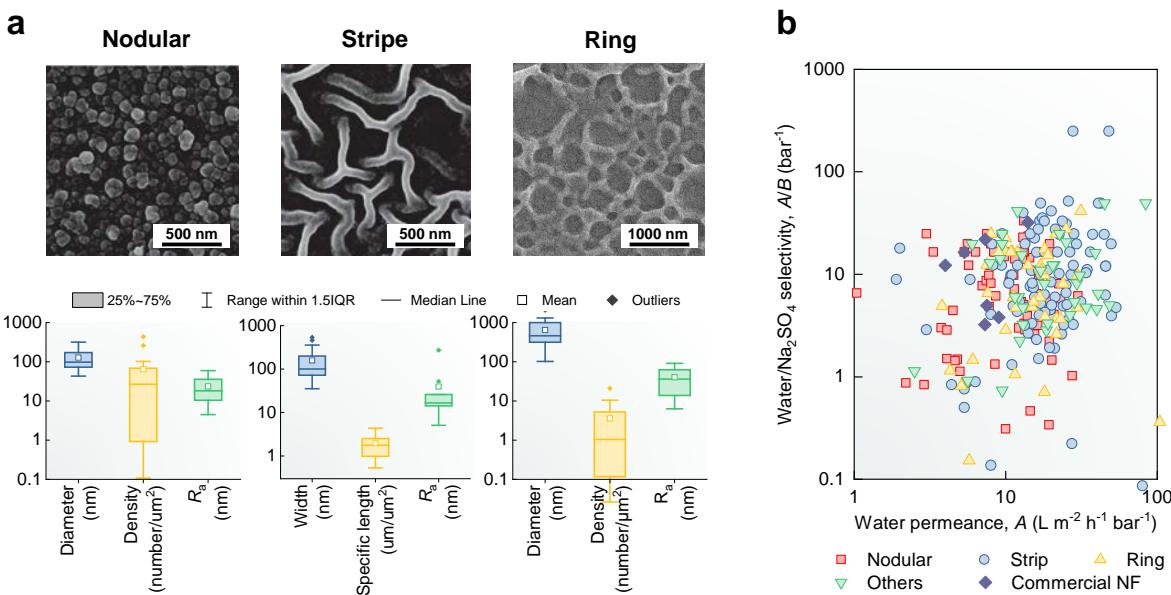
117 **Figure 1.** (a) Typical morphologies of polyamide layer of RO membrane (ESPA3, formed by
 118 MPD and TMC) and NF membrane (NF270, formed by PIP and TMC).³⁰ (b) Number of peer-
 119 reviewed publications on PIP-based NF membranes with crumpled morphologies (incomplete
 120 data for the Year 2022). (c) Water/Na₂SO₄ selectivity (A/B) vs. water permeance (A) for PIP-
 121 based NF membranes with crumpled morphologies (detailed data are provided in [Table S1](#)).

122 Open dots indicate conventional NF membranes with smooth polyamide layers, and closed dots
123 indicate novel NF membranes with crumpled polyamide layers; the data of crumpled NF are
124 color-mapped based on their published years. The scanning electron microscopy (SEM) images
125 were modified from the previous study³⁰ with copyright permission.

126

127 ■ CLASSIFICATION OF CRUMPLED MORPHOLOGIES, THEIR
128 FORMATION MECHANISMS, AND FABRICATION METHODS

129 Typical Crumpled Morphology of NF Membranes and Their Separation Performance



130

131 **Figure 2.** Classification of crumpled morphologies (a) and their corresponding separation
132 performances (b). Diameter, width, and density (number density for nodular and ring structures,
133 and specific length for stripe structure) of the morphologies were based on the statistics of the
134 SEM images of the previous studies (Table S3); Average roughness (R_a) was based on the atomic
135 force microscope (AFM) results of the previous studies. Separation performances of commercial

136 NF are provided in **Table S4**. The SEM images were modified from the previous studies^{29,31} with
137 copyright permission.

138

139 **Table S1** summarizes crumpled polyamide layers for PIP-based NF membranes reported in
140 previous studies. Specifically, nodular,^{29, 32} stripe,^{29, 33, 34} and ring^{31, 35-37} structures are the three
141 most common morphologies (**Fig. 2**). Other structures, such as fishnet-like and octopus sucker-
142 like structures,^{38, 39} are occasionally represented in some studies (**Fig. S1** provides the SEM
143 images of some examples). Among these morphologies, only the nodular structure is observed in
144 existing commercial membranes,⁴⁰ and other morphologies mostly exist in custom-fabricated
145 membranes in literature papers.

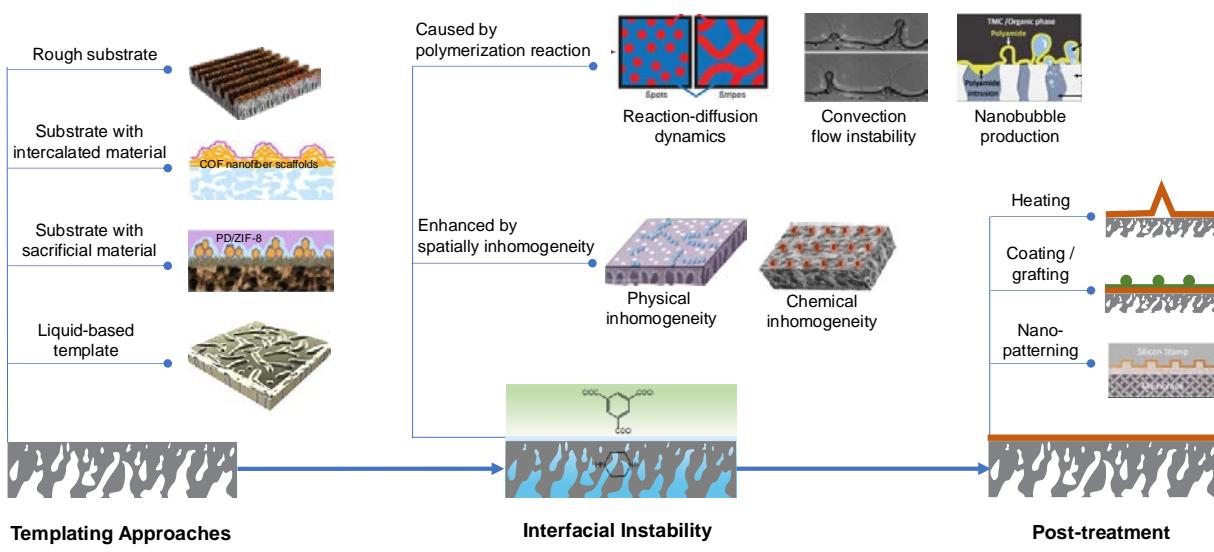
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147 In terms of the nodular structure (**Fig. 2a**), its diameter is often in the range of 50 to 300 nm, with
148 a typical areal number density ranging from 5 to 300 per μm^2 . Based on a limited number of
149 TEM studies,^{29, 32, 41-45} the nodular generally has arc-shaped cross-sections, and the ratio of
150 height to diameter is mostly lower than 1. Possibly because of this low ratio, the average
151 roughness (R_a) obtained using atomic force microscopes (AFM) is often in the range of 10 to 50
152 nm. In terms of stripe structure, the width of the stripes generally ranges from 50 to 400 nm, and
153 the specific length (length/area) ranges from 500-5000 nm per μm . Like the nodular structure,
154 the stripe structures also have low heights,^{29, 46-49} which is also evidenced by the low R_a (5-50
155 nm). Some ring structures are possibly formed by the collapse of canopy structures or large
156 nodular structures.^{50, 51} Therefore, its diameter can reach several μm , while its density is much
157 lower than a typical nodular structure.

158

159 NF membranes with crumpled morphologies often exhibit better separation performance in terms
160 of water permeance and water/solute selectivity than commercially available NF membranes (Fig.
161 2b). Among the common morphologies, the stripe structure appears to be more promising
162 compared with nodular and ring structures. The associated transport mechanisms in crumpled NF
163 membranes will be further discussed under the section “Critical Analysis of Water and Solutes
164 Transport Mechanisms for Crumpled NF Membranes”.

165



166 **Figure 3** Formation of crumpled morphologies of polyamide layers. Templating approach,
167 interfacial instability regulating, and post-treatment could be used before, during, and after the
168 formation of polyamide layers, respectively. The images were modified from the previous
169 studies with copyright permission (rough substrate,⁵² substrate with intercalated material,⁵³
170 substrate with sacrificial material,⁵⁴ liquid-based template,⁵⁵ reaction-diffusion dynamics,²⁹
171 convection flow instability,⁵⁶ nanobubble production,²⁶ physical inhomogeneity,⁵⁷ nano-
172 patterning⁵⁸).

174 **Mechanisms and Fabrication Methods for Crumpled Morphology of Polyamide Layer**

175 The PIP-based polyamide layer on support substrates (e.g., polysulfone membrane) is generally
176 formed through interfacial polymerization of PIP and TMC monomers.^{15, 16, 19} During interfacial
177 polymerization, the substrate is first wetted by a PIP aqueous solution, then immersed in a TMC
178 organic solution. PIP and TMC can react at the aqueous/organic interface and form a polyamide
179 film on the substrate. Post-treatments, such as heating and drying, are often applied to stabilize
180 the polyamide film and further adjust its properties. Based on the protocols of interfacial
181 polymerization, the following strategies could be used to fabricate a crumpled polyamide layer
182 (Fig. 3): 1) using templating approaches to create a rough aqueous/organic interface for
183 interfacial polymerization, so that the formed polyamide film achieves a rough morphology
184 following the aqueous/organic interface; 2) regulating and intensifying the interfacial instability
185 during the reaction of interfacial polymerization; 3) post-processing the formed polyamide layer.

186

187 ***Templating Approaches.*** A rough templating substrate can directly lead to an uneven
188 aqueous/organic interface on the surface of the substrate. Considering the typical thickness of
189 tens of nm for PIP-based polyamide layers,⁵⁹⁻⁶¹ the feature size of the templating substrate should
190 be in the range of hundreds of nm to several μm to affect the formation of polyamide rejection
191 layers. While the typically used polysulfone substrate is relatively smooth,^{20, 62} a few strategies
192 are available to prepare a rough templating substrate. One strategy is patterned membranes.
193 Patterned membranes, often reported for fouling control,⁶³⁻⁶⁵ typically involve fabrication
194 methods such as phase separation micro-molding,^{66, 67} thermal embossing/nanoimprinting^{65, 68, 69},
195 and 3D printing.^{70, 71} Previous studies have constructed patterns such as grooved lines,^{64, 72, 73}
196 pillars,⁷⁴ prism,⁶⁶ pyramid⁷⁵ with dimensions ranging from tens of nm to hundreds of μm . These

197 patterned membranes, when used as substrates, are expected to create aqueous/organic interfaces
198 with regular/periodical morphological features. A second strategy involves the use of scaffolds
199 with rough surfaces, such as non-woven fabrics, stainless steel meshes,⁷⁶ and microfiltration
200 membranes with large pores.^{77, 78} Unlike a patterned substrate, these rough scaffolds usually have
201 an irregular surface morphology. One critical challenge involved in using rough substrates is the
202 increased risks of defect formation in the resulting polyamide rejection layers. For example, if
203 directly conducting interfacial polymerization on rough scaffolds with large pores, the
204 unsupported polyamide film formed over the macropores of the scaffolds is easily broken.^{79, 80}
205 This issue could be potentially addressed by plugging the macropores of the scaffolds with
206 materials of desirable mechanical strength, water permeance, and adhesion force with the
207 scaffold. Some examples include porous protein assemblies⁷⁸ and crosslinked polyvinyl alcohol
208 (PVA).⁷⁶ To achieve a crumpled polyamide layer over the templating substrate, another key
209 consideration is the fidelity of the rough morphology after the interfacial polymerization. Some
210 studies suggested that the fidelity could be improved by decreasing monomer concentrations⁷²
211 and using a layered interfacial polymerization technique.^{74, 81}

212
213 Even with a smooth substrate, one can deposit nanomaterials on its surface to create a rough
214 aqueous/organic interface. Previous studies have deposited nanoparticles^{57, 82-84} and nanofibers,⁵³
215 etc., on substrate surfaces. Common methods for nanomaterial deposition include vacuum
216 filtration,^{45, 54, 85, 86} spraying,^{87, 88} in-situ growth,^{47, 89-92} etc. An ideal deposition is a single layer
217 of nanomaterials with a suitable distance between the individual particles/fibers. The size of
218 nanomaterials may have a major influence: small sizes may minimize the change in
219 morphologies, while large sizes may heighten the risk of defects.⁸⁴ In general, hydrophilic

220 nanomaterials are recommended because they may induce the formation of nanochannels at the
221 interface between the nanomaterial surface and the polyamide matrix.⁹³ For the nanomaterial-
222 based templating approach, the key is to uniformly deposit nanomaterials without aggregation
223 and stacking.⁵⁷ In addition, because the nanomaterial is often water impermeable, the intercalated
224 materials may block the water flow through the resulting NF membrane, causing a compromise
225 in water permeance. The adoption of porous materials, such as porous silica particles,⁹⁴ metal-
226 organic frameworks,^{82, 85, 95} covalent organic frameworks,^{50, 96, 97} and molecular sieves,^{87, 98, 99}
227 may partially address this issue.

228

229 To minimize the impact of intercalated nanomaterials on the performance of NF, one can also
230 use sacrificial materials, such as dissolvable nanoparticles^{54, 100} and salt crystal^{101, 102}, which are
231 readily removed after interfacial polymerization (e.g., by dissolving in water or acid). The
232 removal of these sacrificial materials can create nanovoids in polyamide layers, which can
233 effectively improve the permeance of NF membranes. For example, etching copper nanoparticles
234 using 1% HNO₃ from a copper embedded NF membrane led to quadrupled water flux.¹⁰³

235

236 In addition to solid templates, liquid-based templates may also be used under appropriate
237 interfacial conditions.^{55, 104} For example, to achieve an aqueous template, one could first leave a
238 certain amount of water spread on the substrate surface by tuning rolling pressures and drying
239 conditions. Under specific interfacial tensions, which are adjusted by adding surfactant into
240 aqueous solution and using hydrophilic substrate (including surface-modified and interlayered
241 membrane), the remaining water may form an uneven aqueous/organic interface on the
242 substrate,^{55, 105, 106} resulting in a crumpled polyamide layer after interfacial polymerization.

243

244 **Interfacial Instability.** The interfacial polymerization reaction is inherently associated with
245 instability, which could be utilized to facilitate the formation of crumpled polyamide films. In
246 fact, the interfacial instability is the key to the “ridge-and-valley” morphology of MPD-based
247 polyamide layers.^{19, 107} Currently, the interfacial instability during interfacial polymerization is
248 mostly explained by the following three mechanisms:

249 1) Reaction-diffusion dynamics.^{29, 108, 109} As one of the most famous models of reaction-
250 diffusion dynamics, the activator-inhibitor model is often used to explain the formation of
251 patterns.¹¹⁰ In this model, the activator promotes the synthesis of itself and the inhibitor,
252 while the inhibitor restricts the production of the activator.¹¹⁰ If the diffusion speed of the
253 inhibitor is faster than that of the activator (“local activation and lateral inhibition” proposal),
254 periodic patterns such as spots and stripes (i.e., Turing patterns) may be formed. During the
255 reaction of interfacial polymerization, amine monomers in the aqueous phase firstly diffuse
256 to the organic phase and then react with acyl chloride monomers to form a polyamide film.¹⁹
257 The amine monomer can be regarded as the activator because its diffusion causes the reaction,
258 and the formed polyamide layer can be regarded as the inhibitor because of its self-limiting
259 effect.²⁹

260 2) Convection flow instability.^{56, 111} Interfacial polymerization causes the consumption of
261 monomers and the release of heat, leading to concentration and thermal gradients near the
262 aqueous/organic interface, consequently density gradients and spatially varied interfacial
263 tensions. The density gradient may cause Rayleigh–Bénard convection because gravity tries
264 to pull down the denser liquid.¹¹² The spatially varied interfacial tension may also lead to
265 Marangoni convection because the liquid tends to flow to the place of lower surface

266 tension.¹¹² During interfacial polymerization, these convection flows may result in a
267 fluctuating interface, which might be responsible for the formation of the crumpled
268 polyamide.

269 3) Nanobubble formation. Some recent literature suggested that the crumpled morphology of
270 polyamide layers could be formed by interfacial degassing.¹¹³⁻¹¹⁶ That is, the interfacial
271 reaction between amine and acyl chloride monomers could generate both heat and H⁺, which
272 favors the conversion of dissolved HCO₃⁻ in the aqueous phase (alkaline solution) to release
273 CO₂ nanobubbles. By the confinement of porous substrate, these nanobubbles tend to deliver
274 amine monomers to the reaction front due to the convection under a pressure gradient. In
275 addition, these degassed bubbles could be encapsulated by the nanofilm to tune the
276 polyamide morphology.

277

278 Based on these mechanisms, to enhance the interfacial instability, one could increase the
279 formation of polyamide (inhibitor), enhance thermal and concentration gradients, and/or
280 intensify heat and H⁺ release. Increasing the reaction rate can well-match these goals, e.g., by
281 adding acid acceptor,^{114, 117} increasing reaction temperature,^{31, 118} and adding other co-
282 monomers.¹¹⁹ One can also control the diffusion of PIP (activator) and change the interfacial
283 tension by adding chemicals such as PVA,²⁹ salts,^{120, 121} and surfactants^{34, 122} to the PIP solution,
284 and coating a hydrophilic gel layer on the substrate.¹²³

285

286 The interfacial instability of interfacial polymerization can be enhanced by the spatial
287 inhomogeneity of the reaction. Physical inhomogeneity (i.e., inhomogeneity in monomer storage)
288 of the reaction could be readily achieved using rough substrates (see the section “Templating

289 Approaches”). For example, the valleys of a rough surface may have more PIP monomer
290 storages, and consequently may lead to more violent reactions.^{26, 79, 124} Chemical inhomogeneity
291 could be achieved using a substrate with reactive spots,¹²⁵⁻¹²⁸ and the inhomogeneity may be
292 increased because of the reaction of TMC with these reactive spots. Many studies^{45, 46, 84, 106, 129,}
293 ¹³⁰ reported that the addition of nanomaterial in PIP solution could lead to a crumpled polyamide
294 layer. A possible explanation for this phenomenon is that these nanomaterials intensify the
295 inhomogeneity of the interfacial polymerization, both physically and chemically.^{96, 131, 132}

296

297 **Post-treatment.** Post-treatment is an important step in improving the stability and performance of
298 the NF membrane. Because the polyamide layer may have different thermal expansion and
299 contraction coefficients compared with the substrate, a heating post-treatment may lead to
300 delamination and buckling of the polyamide layer at the micro-/nano-scale,¹⁰⁸ resulting in a
301 rough morphology.^{133, 134} Additionally, surface coating and grafting sometimes cause a rough
302 morphology by adding an additional layer or changing the properties of polyamide layers.¹³⁵⁻¹³⁹
303 Patterning methods can also be used in the post-treatment of the polyamide layer. Because of the
304 thin thickness of the polyamide layer,⁵⁹⁻⁶¹ the dimension of the pattern is generally tens of nm,
305 and previous studies generally used nanoimprinting method.^{58, 68, 140, 141} After the nanoimprinting
306 of commercial NF membranes, their anti-fouling performances are significantly improved (see
307 the section “Critical Analysis of Fouling Propensities of Crumpled NF Membranes”).

308

309 Among the various strategies for the fabrication of crumpled NF membranes, templating
310 approaches can achieve the morphology of a polyamide layer similar to that of the templating
311 substrate, except that the aqueous and nanomaterials-based templating may lead to a stripe

312 morphology after the collapse of the polyamide layer.^{55, 84, 142} By regulating the interfacial
313 instability, the polyamide layer is most likely to form periodic nodular and stripes. With post-
314 processing, especially the patterning method, the polyamide morphology can be further
315 regularized and customized. Although most of the strategies are in the laboratory stage, some of
316 them show the potential for scale-up, with small changes to the existing processing line for
317 interfacial polymerization. For example, by adding a rinsing process to create a PVA interlayer
318 on the substrate, a pilot-scale production line for NF with periodic stripes was successfully
319 established.¹⁰⁵ Additionally, templating approach, interfacial instability regulating, and post-
320 processing are at different steps of the production line, and thus the three methods can be
321 combined to further improve the performance of NF.

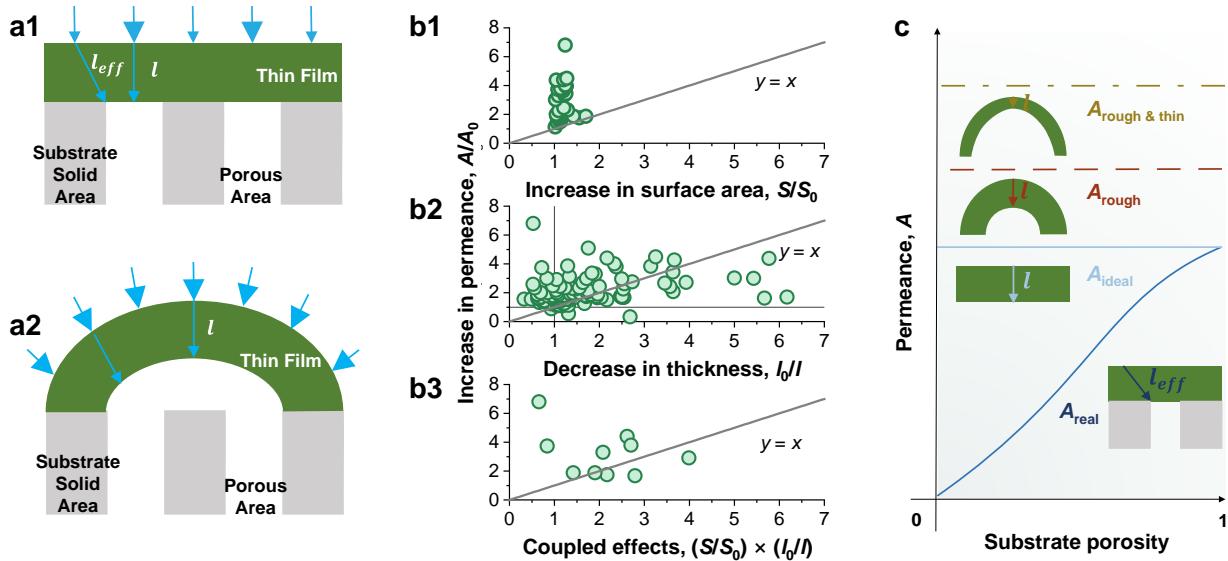
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323 ■ CRITICAL ANALYSIS OF WATER AND SOLUTES TRANSPORT 324 MECHANISMS FOR CRUMPLED NF MEMBRANES

325 Compared to their conventional (smooth) counterparts, TFC NF membranes with crumpled
326 morphologies could have many advantages, including enhanced water permeance and possibly
327 enhanced water/solute and solute/solute selectivity (Fig. 1). Therefore, this section critically
328 analyzes the underlying mechanisms responsible for the improved separation performance with
329 the assistance of conceptual models and literature surveys.

330 **Mechanisms Responsible for Enhanced Water Permeance with Crumpled Morphologies**

331 Several mechanisms can be applied to explain the enhanced water permeance of crumpled NF
332 membranes,^{29, 55, 113} such as an increased effective surface area for filtration, decreased thickness
333 of the polyamide layer, and optimized water transport pathways (Fig. 4).



336 **Figure 4.** Conceptual models (a) for elucidating the mechanisms of enhanced water permeance
 337 of crumpled TFC membranes, where l_{eff} is defined as the actual (effective) water transport
 338 pathways, and l is the intrinsic thickness of the polyamide rejection layer (i.e., the ideal water
 339 transport pathway). (b) Analysis of literature data of crumpled NF membranes in Table S1 with
 340 respect to the effect of surface area ratio (S/S_0), thickness reduction ratio (l_0/l), and their coupled
 341 effects [$(S/S_0) \times (l_0/l)$] on water permeance enhancement. The line of function $y = x$ was
 342 superimposed in each sub-figure. The conceptual model (c) further highlights the benefits of 1)
 343 altered transport path (A_{ideal}) with the increased substrate porosity; 2) increased surface area
 344 (A_{rough} , the superimposed red line); and 3) together with the reduced thickness of the crumpled
 345 polyamide layer ($A_{rough \& thin}$, the superimposed yellow line). Figures a and c were modified from
 346 the previous study²⁶ with copyright permission.

348 **Increased Surface Area of Polyamide Layers.** An intuitive understanding of a crumpled
 349 membrane is that the surface area for water transportation could be significantly enhanced. For

350 example, the striped membrane morphologies (assuming the half-cylinder shape), regardless of
351 the thickness of the polyamide rejection layer, could have the theoretical water permeance
352 enhancement factor of 1.57 (Fig. S2a). For a hemispherical shape of nodular morphology, the
353 theoretical membrane surface area enhancement factor could be two compared to a smooth
354 counterpart (Fig. S2b), potentially translating into doubled water permeance. Although the
355 current literature reports that the characteristic heights of crumpled morphologies are generally
356 low (Fig. 2), crumpled morphologies with higher characteristic heights could result in much
357 higher increases in surface area. However, crumpled morphologies with higher characteristic
358 heights may face the collapse of polyamide film.^{20, 55} Future studies need to explore such
359 phenomena to achieve a compromise between an enhanced surface area of polyamide and its
360 mechanical stability.

361

362 We further performed a comparison between membrane water permeance enhancement and
363 membrane surface area enhancement (characterized by AFM) based on a literature survey (Fig.
364 4b1). These results further corroborate the importance of the increased surface area of crumpled
365 polyamide layers in improving membrane water permeance. It is interesting to note that the
366 increase in membrane surface area alone is not enough to explain the significant flux
367 enhancement observed in the literature. In our analysis, most of the experimental data points are
368 above the theoretical line based on enhanced surface area (i.e., $y = x$), which implies that
369 additional mechanisms may also play important roles.^{29, 55, 113}

370

371 **Decreased Thickness of Polyamide Layers.** In addition to increased membrane surface area, the
372 formation of crumpled morphology is often accompanied by the reduced intrinsic thickness of

373 polyamide layers (Fig. 4b2),^{122, 143-149} which is possibly ascribed to the changes in interfacial
374 polymerization reaction (see the section “Interfacial Instability”) such as inhibited amine
375 monomer diffusion and facilitated polyamide film formation. This reduced thickness of the
376 rejection layer, in some cases up to ~ 6 times, also favors improved water permeance of
377 crumpled NF membranes (Fig. 4b2). Interestingly, the decreased polyamide thickness, often
378 accompanied by the enhanced surface area ratio, could have a synergistic effect on membrane
379 water permeance enhancement, which might explain the close to one order of magnitude
380 enhancement of water permeance for crumpled NF membranes (Fig. 4b3).

381

382 **Optimized Water Transport Pathways.** Compared to the mechanisms of enhanced surface area
383 and reduced thickness of polyamide layers, the mechanism of optimized water transport
384 pathways for crumpled NF membranes has been far less discussed in the literature. Indeed, for
385 the conventional TFC membranes, its separation performance can be severely constrained by the
386 funnel effect,^{26, 150-152} which is often ascribed to the low porosity of the substrate (typically below
387 10%).¹⁵³ As illustrated in Fig. 4a1, the water transport distance away from the substrate pore (l_{eff})
388 of conventional smooth TFC membrane is significantly greater than the thickness of its
389 polyamide rejection layer (l), resulting in significantly higher hydraulic resistance and hence
390 lower water permeance compared to a free-standing polyamide film (an ideal case). To overcome
391 the funnel effect, the crumpled polyamide layer of NF membranes, containing voids that span
392 over multiple substrate pores (Fig. 4a2), could potentially shorten the water transport distance in
393 the rejection layer (in a fashion similar to the inclusion of a high-permeance gutter layer^{151, 154,}
394 ¹⁵⁵). This effect, coined as the self-gutter effect by Tang and coworkers,⁹ can greatly reduce the

395 hydraulic resistance by effectively shortening the water transport pathways (close to the intrinsic
396 thickness of the rejection layer, [Fig. 4a2](#)).

397

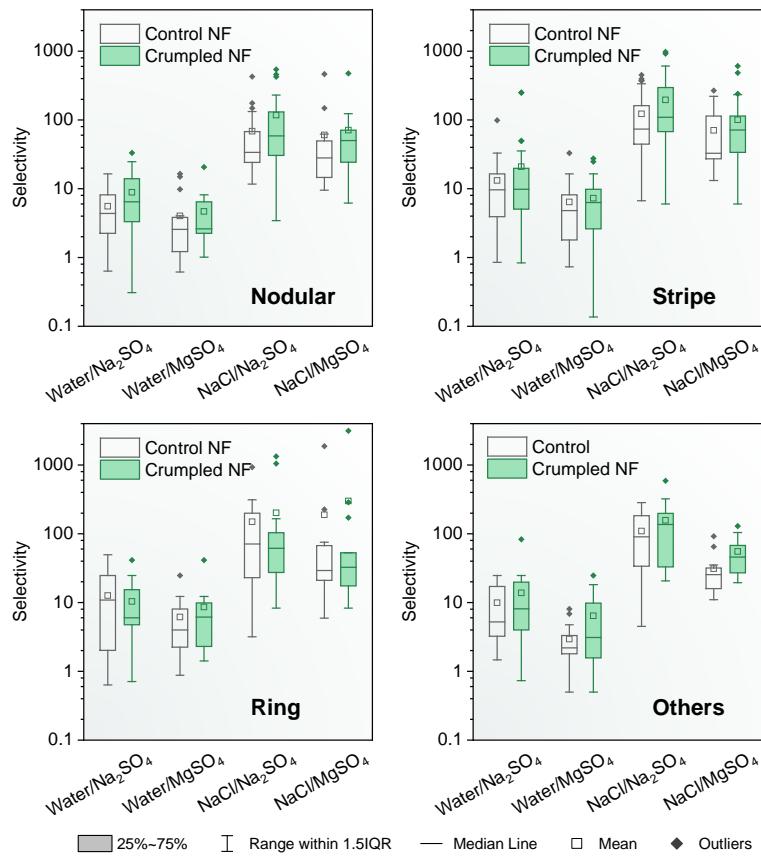
398 To deepen the understanding of this mechanism, [Fig. 4c](#) presents the conceptual model of
399 optimized water transport pathways for improving water permeance. The dark blue line
400 represents the actual membrane water permeance (A_{real}), whereas the light blue line represents
401 the ideal water permeance (free-standing polyamide film, A_{ideal}), with the varying substrates
402 porosities. Due to the funnel effect, the actual water transport distance (l_{eff}) of a conventional
403 TFC NF membrane is significantly longer than the ideal transport distance (l) of a free-standing
404 polyamide film. With the lower substrate porosity, the funnel effect is more severe, resulting in
405 significantly lower water permeance. The crumpled polyamide morphologies, equivalent to the
406 effect of the increasing substrate porosity of a flat polyamide rejection layer, could significantly
407 improve membrane water permeance thanks to the greatly shortened water transport pathways,
408 which approach the ideal water permeance (light blue line). Alternatively, the effect of the
409 nanovoids within the crumpled polyamide rejection layer could be interpreted through their self-
410 gutter effect on shortening the transport path to approach the ideal water permeance.^{9,28} It is also
411 interesting to note that, as an added advantage, the altered water transport pathways tend to result
412 in more uniform flux distribution, which is beneficial to reducing fouling tendency by decreasing
413 the accumulation of foulants in the localized hot spot zone^{151, 156} (see the section “Crumpled
414 Polyamide Film and Local Flux”).

415

416 We further benchmark the theoretical water permeance of the rough NF membrane with an ideal
417 rejection layer (without the effect of substrate, superimposed in red color in [Fig. 4c](#)), which could

418 even successfully exceed the ideal water permeance of the smooth NF membrane due to the
 419 additional benefit of increased filtration area. In reality, a crumpled NF membrane could
 420 simultaneously achieve a reduced thickness of the polyamide layer in addition to optimized
 421 water transport pathways and increased surface areas (line in yellow color, [Fig. 4c](#)), resulting in
 422 the greatest water permeance thanks to these synergistic effects. Overall, our theoretical analysis
 423 is in good agreement with the literature results, where crumpled NF membranes showed up to an
 424 order of magnitude higher water permeance compared to the control. [96, 131, 157-160](#)

425 **Mechanisms Responsible for Enhanced Water/solute and/or Solute/solute Separation of**
 426 **Crumpled Morphologies**



427

428 **Figure 5.** Water/Na₂SO₄, water/MgSO₄, NaCl/Na₂SO₄, and NaCl/ MgSO₄ selectivity of the PIP-
429 based NF membranes with different crumpled morphologies. Detailed data of the box plots are
430 shown in [Table S2](#).

431

432 In addition to the water permeance enhancement, [Fig. 5](#) shows that some crumpled NF
433 membranes may offer enhanced water/solute and/or solute/solute selectivity (e.g., Water/Na₂SO₄,
434 Water/MgSO₄, NaCl/Na₂SO₄, and NaCl/MgSO₄) thanks to the fine-tuned physicochemical
435 properties of the crumpled polyamide layers. As discussed in the section “Interfacial Instability”,
436 the interfacial polymerization reaction rate could be greatly altered, which may further result in
437 changes in membrane crosslinking degree and sometimes the optimized membrane pore size
438 uniformity.^{37, 96, 117, 136, 137, 161, 162} For instance, Liang et al.³⁴ applied sodium dodecyl sulfate (SDS)
439 to manipulate the interfacial polymerization reaction between PIP and TMC, resulting in not only
440 crumpled polyamide morphologies with enhanced water permeance but also more uniform pore
441 size distribution. The resulting NF membrane showed enhanced selectivity towards a wide range
442 of solutes, including mono/di-valent ions and neutral solutes. Interestingly, due to its relatively
443 large pore size in the range of 1 – 2 nm,¹⁶³ the variation of pore size distribution is more effective
444 in enhancing the rejection of divalent ions (e.g., SO₄²⁻, Ba²⁺, and Ca²⁺) or other larger solutes
445 (e.g., glucose and sucrose), and less pronounced in enhancing the rejection of monovalent ions
446 (e.g., Li⁺, Na⁺, and K⁺),^{34, 125, 133, 164-168} and therefore improving its mono-/di-valent ions
447 selectivity (e.g., NaCl/Na₂SO₄ and NaCl/MgSO₄ selectivity in [Fig. 5](#)).

448

449 It is also interesting to note that crumpled NF membranes could also generate localized
450 turbulence to mitigate the localized concentration polarization effect,¹⁶⁹⁻¹⁷¹ which could

451 potentially enhance the water/solute and solute/solute selectivity. Indeed, compared to the
452 smooth counterparts, the crumpled/patterned polyamide films could enhance the localized mass
453 transfer to improve the back diffusion of solute to the bulk,¹⁶⁹ thereby alleviating the
454 concentration polarization and improving both membrane water flux and salt rejection.¹⁷⁰ For
455 example, by comparing the fouling and rejection capability of the crumpled NF membrane with
456 grooves-pattern in both parallel and perpendicular flow orientations, the reduced concentration
457 polarization was revealed.¹⁷¹ Nevertheless, a recent study conducted by Zhou et al.¹⁷² suggested
458 that crumpled morphology may increase the effect of concentration polarization effect, but this
459 increase was compensated by the reduced local flux due to the increase in filtration area. These
460 disparate observations might be partly attributed to the different roughness patterns involved,
461 which calls for more future studies. Although few studies focus on the solute/solute selectivity
462 induced by the mitigated concentration polarization effect of the crumpled membranes, different
463 diffusion coefficients of various ions (e.g., the diffusion coefficient of Na^+ is approximately
464 twice that of Ca^{2+}) could lead to different concentration polarization mitigation degrees (different
465 solutes rejection enhancement), which might result in the enhanced solute/solute selectivity.

466

467 It should also be noted that some fabrication procedures of crumpled polyamide layer may
468 increase the risks of defect formation (e.g., templating approaches).^{98, 173, 174} Additionally, the
469 less-supported ridge of the crumpled layer may be vulnerable to external damage (e.g., high
470 pressure).^{55, 80} When defects are presented in a polyamide layer, although these defect spots can
471 increase water permeance, it is often very risky to result in reduced water/solute and solute/solute
472 selectivity. Future studies should make efforts to minimize defects in the polyamide layer during
473 the fabrication of crumpled NF membranes.

474

475 ■ CRITICAL ANALYSIS OF FOULING PROPENSITIES OF 476 CRUMPLED NF MEMBRANES

477 Membrane fouling is a major obstacle to NF applications. Fouling can cause severe flux losses
478 that need to be restored by physical/chemical cleaning. Fouling of NF membranes is often
479 associated with the deposition of organic substances and the formation of biofilm on membrane
480 surfaces,¹⁷⁵⁻¹⁷⁷ which can be greatly influenced by foulant-membrane interactions and
481 hydrodynamic conditions near the membrane surface.^{178, 179} A crumpled membrane surface can
482 affect both foulant-membrane interactions and hydrodynamic conditions, thus showing
483 significant impacts on membrane fouling.

484

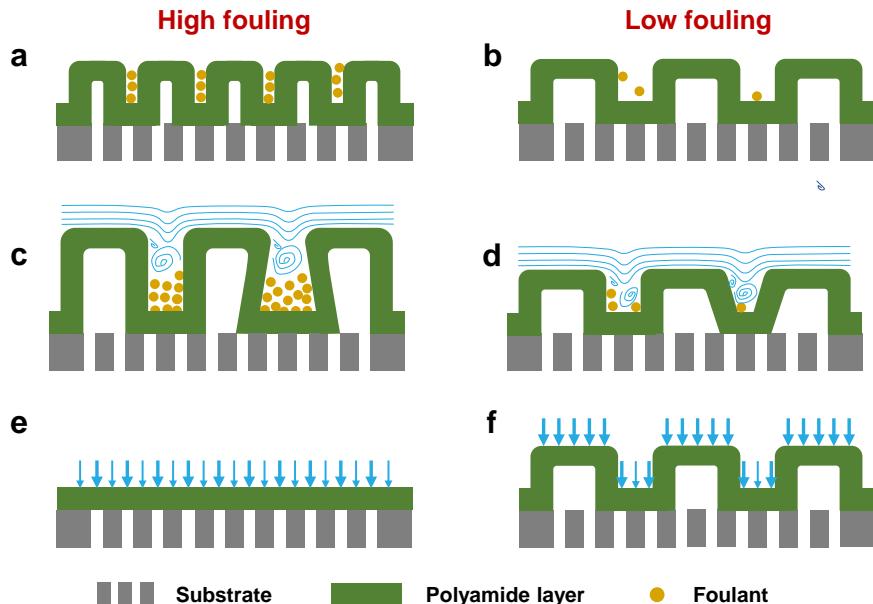
485 **Surface Roughness and Foulant-membrane Interaction**

486 A crumpled surface increases the roughness of a membrane. In the context of RO, since modern
487 polyamide TFC RO membranes typically show a “ridge-and-valley” rough surface,^{20, 60} researchers have long been focusing on the relationship between roughness and fouling from the
488 perspective of foulant-membrane interaction. Elimelech and co-workers^{180, 181} found that a
489 polyamide membrane with high roughness had a more severe colloidal fouling (silica particles
490 with 0.1 μm in diameter), because the colloids were preferentially deposited in the valleys of the
491 membrane. In a follow-up paper, by analyzing the interaction between colloidal particles and
492 membrane surface using Derjaguin-Landau-Verwey-Overbeek (DLVO) theory, these authors
493 attributed the preferential colloidal deposition to the lower repulsive energy barrier at the valleys
494 of the membrane surface.¹⁸² Similar conclusion was also obtained by Bowen et al.,¹⁸³ who found

496 much higher adhesion forces at the valleys of RO membranes using an AFM equipped with silica
497 colloidal probes (4.2 μm). These pioneering studies imply that surface roughness increases the
498 foulant-membrane interaction, especially in the valley region of a membrane, thereby increasing
499 membrane fouling.

500

501 However, some recent studies suggest that enhanced foulant-membrane interactions only occur
502 when the size/shape of the foulant and the valley are comparable (Fig. 6a). For example,
503 Chuning et al.¹⁷⁹ found that the attachment of *S. epidermidis* cells (grape-like shape, $\sim 1 \mu\text{m}$ in
504 diameter) increased when the polyamide membrane surface became rougher, while that of *E. coli*
505 cells (rod shape, $\sim 3 \mu\text{m}$ in length) decreased. The authors attributed this result to the slightly
506 smaller size of *S. epidermidis* than the size of valleys (0.5-3 μm), which enabled *S. epidermidis*
507 to be trapped in these valleys. When the size of foulants is much smaller than that of the valley,
508 the rough membrane “appears smooth” to such small-size foulant (Fig. 6b), and thus, the foulant-
509 membrane interaction may be hardly affected by the roughness.^{184, 185} Consistent with this, a
510 recent study demonstrated that surface roughness had limited influence on the bovine serum
511 albumin (BSA, $\sim 7 \text{ nm}$) fouling for TFC membranes with well-controlled roughness.¹⁸⁶ When the
512 size of foulants is larger than that of the valley, some studies suggested that the foulants-
513 membrane interaction may be reduced by the decreased contact area.^{74, 187, 188}



529 these patterns could effectively reduce colloidal fouling,^{75, 191} organic fouling,^{68, 192, 193} and
530 biofouling.^{66 74} Through particle tracking techniques and computational fluid dynamics (CFD)
531 modeling, several studies show that the ridges of the pattern have a higher shear stress^{75, 194} and
532 the valleys of the patterns can form vortices.¹⁹⁴⁻¹⁹⁶ As a result, a properly designed pattern can
533 create favorable hydrodynamic environments to effectively mitigate foulant deposition.

534

535 Several points should be noted for more effectively increasing local shear stress with the surface
536 patterns. First, hydraulic stagnant spots should be minimized. Surface patterns, while promoting
537 localized turbulences, may also introduce some stagnant spots, especially at the shaded corners
538 and deep valleys of crumpled surfaces (Fig. 6c). An important reason for the high fouling
539 tendency of rough polyamide TFC RO membrane is the existence of some stagnant regions in
540 their “ridge-and-valley” morphology.^{179, 181} Second, well-designed topographies and dimension
541 can achieve better anti-fouling properties.^{67, 197, 198} For example, it was experimentally
542 demonstrated that 45°-rotated pyramid patterns were more effective than pyramid and reverse-
543 pyramid patterns in reducing particle deposition.⁷⁵ The sharkskin-mimetic pattern has an
544 optimized space of 2 μm to mitigate biofouling^{185, 199} with the prevention of biofilm by the
545 enhancement of primary and secondary flow.^{81, 200} Third, flow characteristics have important
546 influences on the anti-fouling performance of patterns. In general, under a high crossflow
547 velocity, large patterns are more effective than small ones for controlling particle deposition.¹⁹⁶
548 Additionally, fouling rates are lower when the flow direction is perpendicular to the lines of
549 grooved patterns, while physical washes are more effective when the flow direction is parallel to
550 the pattern lines.^{191, 201} In addition to the well-defined patterns using the templating or post-
551 nanoimprinting method, other fabrication methods may lead to random surface morphologies, as

552 shown in Fig. 2, and the effect of these morphologies on the local shear stress needs to be further
553 investigated.

554

555 **Crumpled Polyamide Film and Local Flux**

556 It is well accepted that membrane fouling is promoted at a higher flux because of 1) higher
557 foulant loadings, 2) greater hydraulic drag on foulants, and 3) more severe concentration
558 polarization.^{178, 202} Membrane fouling rate is nearly zero when the flux is lower than a threshold
559 value (i.e., critical flux),²⁰³ and may exponentially increase with flux when it is higher than the
560 threshold value.²⁰⁴ In most scientific studies and practical applications, the generally mentioned
561 “flux” is the macroscopically observed average flux of membrane coupons or membrane
562 modules. However, the microscopic local flux, which is more closely related to fouling, could
563 vary at the different locations of membranes.¹⁵¹ For a membrane with non-uniform local flux,
564 although the low-local-flux region has lower fouling, the high-local-flux region has much higher
565 fouling due to the non-linear relationship between fouling rate and flux, and consequently the
566 higher overall fouling.²⁰⁵

567

568 In a smooth polyamide layer, the hydraulic resistance is higher in the regions above substrate
569 walls (because of the longer water transport pathway, Fig. 4a1), and that is lower in the region
570 above the substrate pores.²⁰⁶ Consequently, typically smooth NF membranes tend to have high
571 non-uniformity of local flux, featuring much higher local flux over pore areas (Fig. 6e).^{151, 156}
572 Such non-uniform flux distribution could become even worse for substrates of lower porosities.
573 When the polyamide layer becomes crumpled, the total filtration area increases (Fig. 4b). More
574 importantly, the self-gutter effect leads to a more uniform local flux distribution (Fig. 6f), as

575 experimentally confirmed through tracer filtration tests (e.g., using golden nanoparticles).^{29, 151}
576 With the lower and more uniform local flux, membrane fouling can be greatly reduced. This
577 reason is regarded as the main driver for fouling reduction with crumpled membranes in some
578 studies,⁷³ because of the huge impact of flux on membrane fouling.

579
580 In short, although a smooth polyamide film generally has a low fouling propensity, a crumpled
581 polyamide film with well-designed morphologies could potentially out-perform its smooth
582 counterpart as a result of the associated antifouling mechanisms such as the enhancement of local
583 shear and the reduction of local flux. In addition to membrane fouling, inorganic scaling could
584 also be influenced by surface morphologies.^{207, 208} A rough surface often has a higher scaling
585 potential, possibly because of the favorable formation/deposition of scaling nuclei at the
586 valleys^{209, 210} and the enhanced concentration polarization at the hydraulic stagnant spots.^{172, 179}
587 However, similar to membrane fouling, membrane scaling may also be mitigated by a well-
588 designed crumpled morphology. For example, with a crumpled polyamide, the enhancement of
589 local shear and the reduction of local flux may promote the detachment of scaling nuclei and
590 crystals,^{207, 211} thereby inhibiting the development of scaling.

591
592 **■ ENVIRONMENTAL IMPLICATIONS AND RESEARCH OUTLOOK**

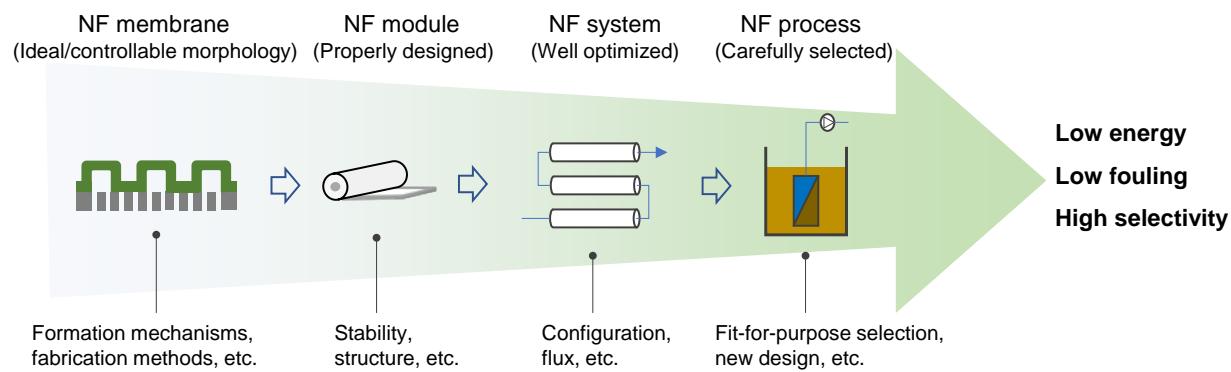
593 As we have discussed the formation, transport mechanisms, and fouling behavior of crumpled
594 NF membranes, we further propose that the ideal crumpled morphology of polyamide film
595 should possess 1) large surface areas (e.g., high aspect ratios of the surface roughness features)
596 and thin thickness for improving the theoretical water permeance, 2) high interconnectivity for
597 internal voids in the crumpled NF membranes (e.g., more optimized water transport pathways for

598 approaching the ideal water permeance and enhanced membrane anti-fouling properties), 3)
599 patterned or rough surface to create localized turbulence, and 4) excellent mechanical strength.
600 To achieve this ideal/controllable morphology, a better understanding of the mechanisms of the
601 formation of crumpled morphology is needed. Although some existing formation models shed
602 light on the mechanisms in generating crumpled polyamide layers, it is still a long way to
603 achieve a quantitative prediction to guide the fine-tuning of the detailed morphological features.
604 Furthermore, since the state-of-the-art separation performance of crumpled NF membranes
605 (mostly at bench scales) has been dramatically improved compared with the commercial
606 counterparts (Fig. 2), subsequent efforts should focus on their long-term stability and scale-up.

607
608 To scale up the crumpled NF, defect-free membranes with large areas should be first fabricated,
609 which need simple and controllable fabrication protocols.²¹² More importantly, with these highly
610 permeable NF membranes, researchers also need to focus on the better translation of high-
611 performance membranes to more efficient processes. For example, a recent study²¹³ highlighted
612 the high permeance NF membrane may not automatically guarantee low energy consumption,
613 nor does a highly selective membrane guarantee better permeate water quality. Therefore, one
614 needs to optimize the membrane module, system, and process to fully unleash the potential of
615 crumpled NF for simultaneously achieving low energy consumption, high product water quality,
616 and a better system flux distribution to avoid fouling issues (Fig. 7). For example, newly
617 designed spacers and flow channels to match crumpled morphologies, multi-stage inter-pumping
618 design or closed-circuit system,²¹⁴ and submerged NF membrane process.²¹⁵ In addition to water
619 permeance, membrane selectivity is also very important for target pollutant removal. Even
620 though crumpled NF membranes may exhibit enhanced selectivity for water/solute and

621 solute/solute, further studies are still needed to improve/tailor the selectivity for specific
622 applications.

623



624

625 **Figure 7.** Schematic diagrams of outlooks and future perspectives of crumpled NF membranes.

626 NF membranes with ideal/controllable morphologies are pursued with the better understanding
627 of morphology formation and the development of simple and controllable fabrication protocols.
628 Beyond membrane fabrication, researchers also need to optimize membrane modules, systems,
629 and processes to fully unleash the potential of crumpled NF for achieving low energy
630 consumption, low membrane fouling, and high selectivity.

631

632 **ACKNOWLEDGMENT**

633 This work was jointly supported by a grant from the Natural Science Foundation of China
634 (52070147) and a grant from the Research Grants Council of the Hong Kong Special
635 Administration Region, China (SRFS2021-7S04). Lu Elfa Peng is supported an RGC
636 Postdoctoral Fellowship from the Research Grants Council of the Hong Kong Special
637 Administration Region, China (PDFS2223-7S02).

638

639 **ASSOCIATED CONTENT**

640 **Support information**

641 Support information of this manuscript can be found online. The support information provides 1)
642 Examples of the polyamide layers with other morphologies; 2) increases in the surface area of
643 polyamide layers with simplified stripe and nodular morphologies; 3) classifications, fabrication
644 methods, and separation performances of the PIP-based NF membranes with crumpled
645 morphologies; 4) selectivity of the PIP-based NF membranes with crumpled morphologies; 5)
646 topographical features of the morphologies; and 6) separation performances of several
647 commercial PIP-based NF membranes.

648

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